

Prepared For: CEMCO 13191 Cross Road Parkway, Suite 325 City of Industry, CA 91746



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ASTM E90-09 (2016): Laboratory Measurement of Airborne Sound Transmission of Building Partitions and Elements

- Result Summary: STC 51
- Specimen: Wall Assembly

Method: ASTM E90-09 (2016)

- Test Site: North Orbit Acoustic Laboratory Facility 512 5th Street NW Dyersville, IA 52040
- Technician: D. Berg
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Suppliment to Test Report 18-0762

David M. Berg Laboratory Manager

Heide Gross Laboratory Quality Manager

Two signatures are required for an official laboratory test report. Copies without signatures are considered to be for reference only.



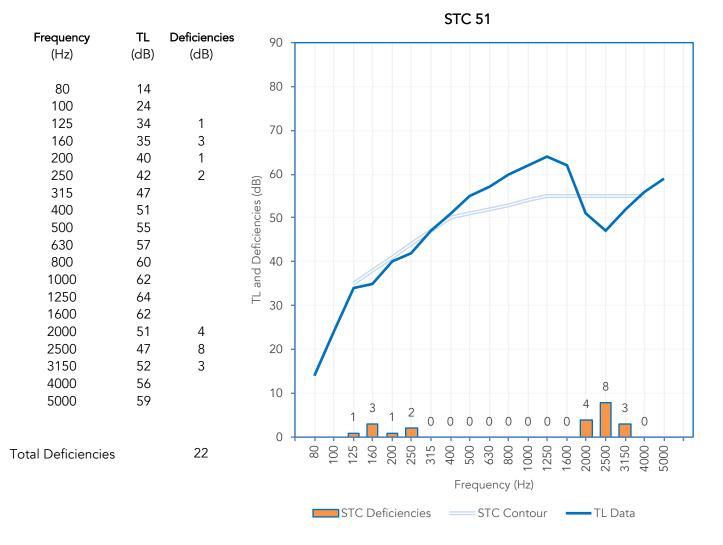


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ASSEMBLY ELEMENTS: (From Source Room Side to Receive Room Side)

Sheathing Sheathing	5/8" Type X gypsum wallboard (vs); 1.625" #6 type S screws spaced 12" OC perimeter and 16" OC field 5/8" Type X gypsum wallboard (v); 1" #6 type S screws spaced 12" OC perimeter and 16" OC field
Framing	3-5/8" CEMCO Viper-X (VXS) 19 mil (20 EQ) studs spaced 24" OC
Insulation	3-1/2" fiberglass insulation batts (R13)
Sheathing	5/8" Type X gypsum wallboard (vs); 1" #6 type S screws spaced 8" OC perimeter and 12" OC field





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### SPECIMEN DESCRIPTION

The specimen is a wall assembly and it's elements are described below with results on page 2. Detailed information regarding the specimen is found in Appendix C on pages 6 and 7.

### INSTALLATION AND DISPOSITION

The wall assembly was originally constructed on July 24, 2018 at the Dyersville acoustic laboratory location.

Qualfied representatives from North Orbit Acoustic Laboratories observed the installation process and inspected all major building elements when completed and prior to testing.

#### FILLER WALL

A high transmission loss double stud filler wall was constructed in the entire 20' x 12' test opening. The filler wall consisted of two 1.5" x 7.5" x 12' wood bottom and top plates separated by approixmately 3" of air space. 1.5" x 3.5" wood studs were placed at 24" OC in each frame. The resulting cavity was filled entirely with fiberglass batt insulation. Four layers of Type C gypsum wall board (GWB) were attached to the outside of the frames on both sides. The GWB on the north side of the filler is mounted on reslient clips and 7/8" hat channel at 16" OC. The GWB on the south side is directly attached to the frame. The filler wall assembly was tested and the results retained for use in composite wall corrections. The filler wall was then modified to provide a 12' x 8' decoupled opening to accomodate tests in this series.

#### TEST METHODS

Methods follow the published standards listed below. All values derived from single-direction transmission loss measurements.

ASTM E90-09 (2016): Standard Test Method for Laboratory Measurement of Airborne Sound Transmission Loss of Building Partitions and Elements

#### ASTM E413-16: Classification for Rating Sound Insulation

All results reported herein were derived from tests performed in full accordance with test method ASTM E90-09 (2016). The laboratory and measurement systems fully meet all requirements of the test standard and the requirements of ASTM E90-09 (2016) Annex A2: Qualification of room sound fields and microphone systems used for sampling.

North Orbit Acoustic Laboratory (NOAL) is accredited through A2LA certificate number 4240.01 for this test procedure. This test report relates only to the item(s) tested. This report shall not be used to claim product certification, approval, or endorsement by North Orbit Acoustic Laboratories or A2LA.

## CONFIDENTIALITY

The client has full control over this information and any release of information will be only to the client. The specific testing results are deemed to be confidential exclusively for the client's use. Reproduction of this report, except in full, is prohibited.





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## APPENDIX A: MEASUREMENT SETUP

#### ENVIRONMENT

Temperature: Relative Humidity:	69 °F 61 %	21 °C			
SPECIMEN AREA					
Specimen Area:	96.0 ft <sup>2</sup>	8.92 m²			
CHAMBER VOLUME - AIRBORNE TRANSMISSION					

Source Room	7079.0 ft <sup>3</sup>	200.5 m³
Receive Room	7828.8 ft <sup>3</sup>	221.7 m <sup>3</sup>

#### **INSTRUMENTATION**

Description	Brand	Model	Serial Number
Analyzer	Sinus	Apollo	7510
Software	Sinus	Samurai	ver. 2.8.1
Microphone	Brüel & Kjær	4166	1620281
Microphone	Brüel & Kjær	4166	1620312
Preamplifier	Brüel & Kjær	2669	2025373
Preamplifier	Brüel & Kjær	2669	2083679
Rotating Boom	Brüel & Kjær	3923	1263440
Rotating Boom	Brüel & Kjær	3923	2705113
Calibrator	Brüel & Kjær	4231	2162880
Loudspeaker	Mackie	SA1501	PP14915
Loudspeaker	Mackie	SA1501	PP14940





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## APPENDIX B: CALCULATION RESULTS

Freq. Band	Spec TL	Data Flags	0.95 Conf.	Flanking Limit	STC Defic.	Rw Defic.
(Hz)	(dB)	(see below)	Δ TL (dB)	(dB)	(dB)	(dB)
25		1				
32						
40						
50	14.3		3.78	40		
63	14.4		3.28	45		
80	14.4		4.57	46		
100	24.1		2.47	49		7.9
125	34.0		2.21	55	1	1.0
160	34.9		1.12	58	3	3.1
200	40.2		1.30	62	1	0.8
250	42.1		1.24	65	2	1.9
315	47.1		0.79	68	-	-
400	51.1		0.66	71	-	-
500	54.5		0.51	74	-	-
630	57.3		0.45	76	-	-
800	60.1		0.44	79	-	-
1000	62.3		0.38	81	-	-
1250	63.5		0.48	84	-	-
1600	61.7		0.27	83	-	-
2000	51.1		0.34	82	4	3.9
2500	47.2		0.35	86	8	7.8
3150	51.5		0.61	90	3	3.5
4000	55.6		0.57	89	-	
5000	59.1			86		
6300						
8000						
10000						
Total deficiencies below STC contour (dB) 22					22	
STC contour [ASTM E413] 51						
Total deficiencies below Rw contour (dB)					29.9	
Rw contour [ISO 717/1]						51.0

Note: 95% confidence intervals for TL measurements from room qualification data. ASTM E1289 reference sample and repeatability data available upon request. The standard deviation of reproducibility is stated in ASTM E90 as <2 dB for frequencies from 125 Hz to 4 kHz. Flanking Limit derived from chamber flanking study. Extended frequency results below 80Hz and above 5000Hz are for reference only.





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## APPENDIX C: SPECIMEN ASSEMBLY DESCRIPTION

Overall Mass 705.20 lb [319.87 kg]

Surface Weight 7.35 PSF [35.87 kg/m<sup>2</sup>]

Building Element	Mass lb (kg)	Surface Weight PSF (kg/m2)	
5/8" Type X gypsum wallboard (vs); 1.625" #6 type S screws spaced 12" OC perimeter and 16" OC field	214.8 [97.4]	2.24 [10.92]	
5/8" Type X gypsum wallboard (v); 1" #6 type S screws spaced 12" OC perimeter and 16" OC field	214.8 [97.4]	2.24 [10.92]	
3-5/8" CEMCO Viper-X (VXS) 19 mil (20 EQ) studs spaced 24" OC	40.0 [18.1]	0.42 [2.03]	
3-1/2" fiberglass insulation batts (R13)	21.4 [9.7]	0.22 [1.09]	
5/8" Type X gypsum wallboard (vs); 1" #6 type S screws spaced 8" OC perimeter and 12" OC field	214.2 [97.2]	2.23 [10.89]	



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# APPENDIX C: SPECIMEN ASSEMBLY DESCRIPTION (CONTINUED)

## FRAMING

Framing was constructed on 07-23-18 and was retained from previous tests in the series.

A steel stud frame was constructed in the perimeter of the laboratory test specimen opening. The frame consisted of CEMCO Viper-X (VXT),19 mil designated thickness (20 EQ) 3-5/8" x 1-1/4" bottom tracks, CEMCO TAB Track (TAB250), 33 mil designated thickness (20 ga.) 3-5/8" x 2-1/2" tabbed top tracks and seven CEMCO Viper-X (VXS) 19 mil designated thickness (20 EQ) 3-5/8" x 1-7/16" studs installed 24" on center (OC). The bottom tracks and studs were fastened together with two 7/16" #7 type screws at each intersection. The perimeter of the frame was sealed at the specimen opening sides and bottom with non-hardening acoustic sealant.

# INSULATION

Fiberglass batts were friction fit into each of the stud cavities. The batts were 24" wide and 3-1/2" thick with an R-value of R-13.

# SHEATHING

**Source Side**: The source room top frame edge was fitted with a CEMCO Sound Gasket. The Sound Gasket's 1-1/2" x 1/2" vinyl profile had a bubble gasket at the inner (frame side) top edge. The 1-1/2" leg was attached to the top track leg with #8 1/2" S-12 screws 36" OC. Two layers of gypsum wallboard panels were applied to the source room side of the framing. A 1/2" deflection gap was left at the top edge of both layers of gypsum wallboard. Base layer: 5/8" Type X gypsum wallboard panels were applied parallel to the studs. The panels were attached to the frame (except top track) with 1", #6 type S drywall screws at 12" OC at the perimeter and 16" OC in the field. Face layer: 5/8" Type X gypsum wallboard panels were applied parallel to the studs. The panels were attached to the frame with 1-5/8", #6 type S drywall screws at 12" OC at the perimeter and 16" OC in the field. Face layer: 5/8" Type X gypsum wallboard panels were applied parallel to the studs. The panels were attached to the frame with 1-5/8", #6 type S drywall screws at 12" OC at the perimeter and 16" OC field. Joints were staggered 24" as to offset on each layer. **Receiver Side**: The receiver room top frame edge was fitted with a CEMCO Sound Gasket. The Sound Gasket's 1-1/2" x 1/2" vinyl profile had a bubble gasket at the inner (frame side) top edge. The 1-1/2" leg was attached to the top track leg with #8 1/2" S-12 screws 36" OC. One layer of 5/8" Type X gypsum wallboard panels were applied parallel to the studs. A 1/2" deflection gap was left at the top edge of the gypsum wallboard. The panels were attached to the frame (except the top track) with 1", #6 type S drywall screws at 8" OC at the perimeter and 12" OC in the field. Joints were staggered 24" as to offset on opposite sides of the frame.

The panels were placed at installation so equal gaps were maintained. Gaps were less than 3/8", except deflection gap which was 1/2" maximum. The seams were sealed on the source and receiving room sides with non-hardening acoustical sealant. In addition, the sides and bottom of both sides of the specimen was sealed with 2" wide, polypropylene tape and 7/8" dense putty tape.





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## APPENDIX D: SINGLE-NUMBER CALCULATION TO ISO 717-1

Freq.	Ri	Ref	Unfav.	Li1	Li1 - Ri	Li2	Li2 - Ri
Band	(Ri ≡ TL)	Curve	Deviat.	Spectrum	Level	Spectrum	Level
(Hz)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)
50	14.3						
63	14.4						
80	14.4						
100	24.1	32.0	7.9	-29.0	-53.1	-20.0	-44.1
125	34.0	35.0	1.0	-26.0	-60.0	-20.0	-54.0
160	34.9	38.0	3.1	-23.0	-57.9	-18.0	-52.9
200	40.2	41.0	0.8	-21.0	-61.2	-18.0	-58.2
250	42.1	44.0	1.9	-19.0	-61.1	-15.0	-57.1
315	47.1	47.0	-	-17.0	-64.1	-14.0	-61.1
400	51.1	50.0	-	-15.0	-66.1	-13.0	-64.1
500	54.5	51.0	-	-13.0	-67.5	-12.0	-66.5
630	57.3	52.0	-	-12.0	-69.3	-11.0	-68.3
800	60.1	53.0	-	-11.0	-71.1	-9.0	-69.1
1000	62.3	54.0	-	-10.0	-72.3	-8.0	-70.3
1250	63.5	55.0	-	-9.0	-72.5	-9.0	-72.5
1600	61.7	55.0	-	-9.0	-70.7	-10.0	-71.7
2000	51.1	55.0	3.9	-9.0	-60.1	-11.0	-62.1
2500	47.2	55.0	7.8	-9.0	-56.2	-13.0	-60.2
3150	51.5	55.0	3.5	-9.0	-60.5	-15.0	-66.5
4000	55.6						
5000	59.1						
		Sum =		RA,1 =	48.4	RA,2 =	
		RW =	51.0	C =	-3	Ctr =	-8.0

Rw (C ; Ctr) = 51 (-3 ; -8) Rw (C ; Ctr ; C50-3150 ; Ctr,50-3150) = 51 (-3 ; -8 ; -8 ; -19)

Rw (C ; Ctr ; C100-5000 ; Ctr,100-5000) = 51 (-3 ; -8 ; -2 ; -8) Rw (C ; Ctr ; C50-5000 ; Ctr,50-5000) = 51 (-3 ; -8 ; -7 ; -19)

Calculations in ISO 717-1 are performed based on assumed equivalency of the ASTM and the corresponding ISO test methods. The test herein is performed according to the ASTM standards. NOAL *does not* hold accreditation for ISO 140 or ISO 717 under their scope of accreditation.

The spectrum adaptation terms C and Ctr characterize performance against two specific sound sources, A-weighted pink noise and A-weighted traffic noise respectively. The standard ISO 717-1 includes a discussion of "Use of Spectrum Adaptation Terms" in Annex A (informative).

Each spectrum adaptation term may additionally be reported with extended frequency bands included. A calculation for the primary frequency range is shown above, but all available extended-frequency calculations were performed to compare against corresponding ratings of other specimens.